# MATE 313 Fall 2019

## Homework #4

# Due: November 28<sup>th</sup>, 2019 (lecture time)

Group submission (up to 3 students per group) is allowed.

#### **Question 1:**

Estimate the energy (in  $J/m^2$ ) of a semicoherent (100) interface between FCC Co precipitate and FCC Cu matrix. Ignore the energy of the coherent regions.

Info:

Energy of a dislocation is  $T = Gb^2/2$  where G is the shear modulus and b is the Burgers vector.

The lattice parameter of Cu is 0.364 nm and that of (cubic) Co is 0.352 nm. Take G = 45 GPa.

#### **Question 2:**

Cu can dissolve in Ag to form a substitutional solid solution. Cu atoms are, however, smaller than Ag atoms and each Cu atom therefore distorts the surrounding Ag lattice, i.e. a coherency strain field effectively exists around each Cu atom. Estimate the misfit strain energy in kJ/mol.

	Radius (nm)	Shear Modulus (GPa)
Ag	0.144	27.8
Cu	0.128	44.7

#### **Question 3:**

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An A-B alloy system contains <u>cube shaped</u>  $\beta$  precipitates of almost pure B with a side length "a" of 11 nm. Based on the information given below, <u>determine whether these precipitates</u> <u>have coherent or non-coherent interfaces</u> with the A-rich  $\alpha$ matrix. State any assumption you will make.

 $a_{\alpha}$  (lattice parameter of  $\alpha$ ) = 0.143 nm

 $a_{\beta}$  (lattice parameter of  $\beta$ ) = 0.151 nm

 $y_{st}$  (structural contribution to the interfacial energy) = 0.45 J/m<sup>2</sup>

 $\mu$  (shear modulus of the matrix) = 25 GPa

#### **Question 4:**

In a material, homogeneous nucleation of  $\beta$  phase in  $\alpha$  phase is found to occur at an undercooling,  $\Delta T = 170^{\circ}C$ .

Given that the  $\alpha$  grain boundary has an energy of 0.66 J/m<sup>2</sup> and the  $\alpha/\beta$  interface has an energy of 0.44 J/m<sup>2</sup>, <u>at what</u> <u>undercooling will heterogeneous nucleation be observed</u> <u>along the grain boundaries?</u>

Assume that the driving force is proportional to the undercooling ( $\Delta$ Gv  $\propto \Delta$ T). Also neglect differences in the density of potential nucleation sites between homogeneous and heterogeneous nucleation.

The formula for the shape factor,  $S(\theta) = 0.5(2 + \cos\theta)(1 - \cos\theta)^2$ 

### **Question 5:**

Assume that a spherical precipitate forms in an age hardening alloy and that the volume-free energy change associated with the formation of a particle is  $-7.3 \times 10^7$  J/m<sup>3</sup>. The surface energy of the interface between the particle and the matrix is 0.44 J/m<sup>2</sup>.

a) Assuming the misfit strain energy to be zero, <u>determine</u> <u>the critical nuclei radius (r\*) and critical energy ( $\Delta G^*$ ) for</u> <u>precipitation.</u>

b) <u>Calculate the number of particles per m<sup>3</sup></u> if the precipitates have a total volume fraction of 1.5% and they are of the same size with a radius equal to the twice of the critical radius size.

c) Calculate the total change in free energy due to the formation of all the precipitates in one m<sup>3</sup>.

**Question 6:** 

For an A-B alloy system with precipitates that are pure element B, a solvus line is described by $log(X_B) = 2.853 - 2.875 \times 10^3/T$ , where $X_B$ is the composition in atomic %.
What is the growth rate (in $\mu$ m/h) at T = 727°C for a matrix composition of X <sub>0B</sub> = 2.5% five minutes after the nucleation has taken place?
Assume 1D growth (e.g. of a slab of precipitate nucleated on a grain boundary). The pre-factor and activation energy for the

diffusion of B in A are  $7.4 \times 10^{-5}$  m<sup>2</sup>/s and 257.4 kJ/mole, respectively.